Preliminary Analysis Of The Effects Of The Application Of Biostabilised Waste On Soil In Terms Of Heavy Metal Accumulation And Leaching

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Abstract

The aim of this work was to evaluate and compare potential impacts related to the accumulation and/or release of heavy metals resulting from the application on soil of different types of stabilized waste. Namely, the following three types of flows were considered: waste produced by aerobic bio-stabilization of municipal solid waste at a Mechanical Biological Treatment (MBT) plant, compost produced either from aerobic composting or from a combination of anaerobic and aerobic bio-degradation processes. After a preliminary characterization of the materials (organic matter content, volatile solid, and heavy metals content), heavy metal accumulation in soil caused by possible long-term application of these organic materials was evaluated by implementing a discretized mass balance based on the total content of the heavy metals in each type of solid matrix investigated. In addition, results of percolation leaching tests performed on each type of material were presented and discussed. Results highlight that although the total content of heavy metals of the three types of materials differed considerably, the MBT waste presenting the highest concentrations, the results of the leaching percolation test were quite similar.

Keywords: aerobic stabilization, anaerobic digestion, MBT waste, compost, metal accumulation, leaching behavior

Introduction

Recently, the European Commission has been strongly promoting the enactment of a circular economic model aimed at preserving natural resources and minimizing landfill utilization. In this framework, Member States have taken actions in order to divert biodegradable municipal waste from landfills and to reduce impacts during their management due to their putrefying nature, with respect to both biogas and leachate emissions. Specifically, two main strategies are adopted for the management of this fraction aerobic and/or anaerobic biodegradation of the source-segregated Organic Fraction of Municipal Solid Waste (OFMSW), with production of compost and digestate, and mechanical–biological treatment (MBT) of residual MSW to produce biostabilised waste, besides waste-derived fuels aimed at energy recovery (Abdullahi et al., 2008). Compost is generally used in agriculture as a fertilizer and for improving the soil’s physical and chemical properties (Westerman and Bicudo, 2005; Hargreaves et al., 2008). Northern European countries such as Denmark, Sweden or Germany admit the utilization of digestate as a soil fertilizer (Möller and Stinner, 2009; Ortenblad, 2002; Rodhe et al., 2006), but this activity is generally allowed only for the separately collected organic fraction of MSW. Differently, the main fate of MBT waste is landfilling due to its higher content of non-biodegradable materials (e.g. plastic pieces) and heavy metals, compared to compost (Di Lonardo et al., 2015). However, the interest in the possibility of recovering MBT waste is increasing (MacLeod et al., 2008), especially considering the large amounts that are being produced in efforts to divert waste from landfills (Farrell and Jones, 2010). One of the possible ways to recover MBT waste is as landfill cover material for promoting vegetation growth (Aungermeier et al., 2011); application to degraded and/or contaminated soils of these organic rich fractions has been also proposed (Farrell and Jones, 2010). To date Italy has a specific regulation for the reuse of biostabilised fractions like compost as soil improvers (D.Lgs. 217/06). Requirements are expressed in terms of total composition (e.g. total content of heavy metals), not leaching behaviour. It is however well established that the potential risks to the environment related to the use or disposal of a material should be assessed also in terms of release when in contact with water; not only total content (van der Sloop et al., 2004).

This study was aimed at assessing and comparing the application on soil of different types of treated bio-waste produced from a Mechanical Biological Treatment plant, an aerobic composting process and from a combination of anaerobic and aerobic biodegradation processes (Pantini et al., 2015; Di Lonardo et al., 2016; Lombardi et al., 2016). To this aim, metal accumulation caused by the long-term application of bio-stabilised waste on soil was assessed by implementing an approach based on a discretised mass balance over time as suggested by the European Compost Network (ECN et al., 2015). In addition, leaching data from percolation tests (Di Lonardo et al., 2016; Lombardi
et al., 2016, Pantini et al. 2015) were analyzed in terms of heavy metal release over time.

Materials and methods

Investigated samples

Three different types of bio-stabilized waste materials were analyzed in this study: MBT waste produced by aerobic bio-stabilization of mechanically selected municipal waste and two types of compost produced from an aerobic composting process (Compost A) and from a combination of anaerobic and aerobic bio-degradation processes (Compost B).

The MBT waste was sampled in a plant that has a maximum treatment capacity of 750 Mg MSW/d. Downstream of a primary mechanical sieving unit at 90 mm, electromagnetic separators remove metals and the biodegradable fraction is sent to a bio-stabilization basin, where forced aeration conditions enhance the aerobic biodegradation of the organic fraction. After around 28 days, the output is mechanically sieved at 20 mm in order to separate the oversize fraction enriched in plastics and inert materials (Di Lonardo et al., 2012).

The Compost A sample was collected from a plant that treats source-segregated organic fractions of MSW (from local markets, restaurants and households) with a maximum treatment capacity of 82 Mg/d. After 28 days at forced aeration conditions, the material was subjected to a ripening stage at natural aeration conditions for 180 days and then sieved at 10 mm.

The Compost B sample was collected from a biodigester/composting plant which likewise treats source-segregated organic fractions of MSW (mainly food and green waste) with a maximum treatment capacity of 120 Mg/d. This plant is made up of two different biodegradation processing stages. Firstly, an anaerobic digestion stage lasting 15 days is carried out for a part of the input waste; then, the digestate output is mixed with the remaining waste and sent to the aerobic composting stage. Downstream of a mechanical sieving unit at 40 mm, the organic fraction remains in bio-cells at forced aeration conditions for 20 days. The bio-stabilized material is kept at natural aeration conditions for 90 days in order to achieve ripening conditions. Secondary mechanical sieving at 10 mm is carried out at the end of the ripening phase. The oversize flows are recirculated at the beginning of the process in order to act as structuring materials during the two biodegradation stages.

Evaluation of metals accumulation in topsoil

Bio-stabilized materials do not contain only nutrients and organic matter, but also a significant quantity of minerals and specifically metal bearing phases. While the organic matter fraction can be mineralized and the nutrients absorbed by plants, the mineral fraction remains permanently, contributing to soil structure. Therefore, mineral components, which remain in the soil over time, cause an increase in soil horizon and contribute in defining its contamination level. In order to evaluate the effect of pollutants accumulation in topsoil resulting from the application of bio-stabilized materials on one hectare of soil, the model presented by the European Compost Network for compost was used (ECN et al., 2015). Specifically, the following equation was considered:

$$C_{Bo,t} = \frac{(C_{Samp} \times M \times 0.1 \times t) + (C_{Bo} \times d \times 1000 \times h)}{(d \times 1000 \times h) + (M \times A_{long} \times 0.1 \times t)}$$ (1)

Where:

- $t$: Period of application [years]
- $C_{Bo}$: Metal concentration in relevant soil horizon [mg/kgTS]
- $C_{Bo,t}$: Metal concentration in relevant soil horizon after t years [mg/kgTS]
- $C_{Samp}$: Metal concentration in the compost [mg/kgTS]
- $h$: Soil horizon thickness [m]
- $M$: Annual application rate [MgTS/ha]
- $A_{long}$: Fraction remaining in the soil over the long term [%]
- $d$: Dry bulk density of soil [g/cm$^3$]

In the mass balance (Equation 1) a soil, with a horizon thickness $h$ of 30 cm and a dry bulk density $d$ of 1.7 g/cm$^3$ was considered (ECN et al., 2015). We assumed an application on soil of 10 Mg/(ha*year) of dry matter of bio-stabilized waste in a period of $t$ consecutive years. The application rate $M$ corresponds to the maximum value allowable for compost in Germany, assumed also in the ECN study (ECN et al., 2015). In order to take into account of the long-term application of the materials to soil, it should be considered that stable fractions contribute to long-term soil structure. In this study, the fraction remaining after long-term application ($A_{long}$) was assumed to be equal to the mineral fraction of the material plus the portion resistant to biological degradation. The former was assumed to be equal to 82.5% of the ash content, while the latter was estimated by assuming that 26% of the organic matter, expressed as VS, contained in the bio-stabilized waste remains in the soil over the long term (Deller et al., 2008). $C_{Bo}$ and $C_{Samp}$ represent the initial metal concentrations in soil and in the bio-stabilized waste respectively, whereas $C_{Bo,t}$ corresponds to the concentration in the soil horizon after t years of application of the biostabilised materials.

Leaching behavior

In our previous studies, we specifically investigated the leaching behavior of the waste materials considered in this work (Pantini et al., 2015, Lombardi et al., 2016, Di Lonardo et al., 2016), as shown in Table 1, where the
contents of organic matter (volatile solids and total organic carbon) and heavy metals are also reported. Although the three samples proved quite different especially in terms of heavy metal contents, an interesting finding was that the metals leaching kinetics as a function of the L/S ratio seemed to be governed by the same mechanisms (Pantini et al., 2015, Di Lonardo et al., 2016). To evaluate how much water could come in contact with the material in the application area, the empirical model proposed by Connor et al., (1997), that allows to estimate the net infiltration rate as a function of the average annual rainfall \( P \) (cm/year) and of the predominant soil type (sand, silt or clay) was used (Equation 2 for silty soil). The net infiltration rate \( I_f \) was utilized to estimate, for the application area \( A \), how much water could infiltrate in the soil after every year (Equation 3) and how long does it take to pass through the soil horizon thickness (Equation 4).

\[
I_f = 0.0009 \times (P)^2 \quad (2)
\]

\[
Q_{\text{inf}} = I_f \times A \times 10 \quad (3)
\]

\[
t_{\text{inf}} = \frac{h}{I_f} \quad (4)
\]

Where:
- \( I_f \) Net infiltration rate \( \text{cm/year} \)
- \( A \) Area of infiltration \( \text{m}^2 \)
- \( Q_{\text{inf}} \) Water that infiltrates in area \( A \) \( \text{l/year} \)
- \( t_{\text{inf}} \) Time to pass through \( h \) \( \text{years} \)

The net infiltration \( I_f \) was evaluated by considering an annual precipitation value \( P \) of 77.2 cm/year, assumed by the European average rainfall in 2008 (http://www.nationmaster.com).

This value was used to calculate how much time the topsoil, represented by the first 30 cm of soil and the accumulated biostabilised material, need to come in contact with rainfall to reach the investigated liquid to solid ratios adopted in the percolation tests (Table 3).

**Results and discussion**

**Metals accumulation in soil**

Figure 1 shows how the concentration in the relevant soil horizon changes over time.

Since nutrients uptake by plants is not considered in this work, the \( A_{\text{long}} \) values were found to be equal to 51.9 % for MBTW, 44.5 % for Compost A and 51.4 % for Compost B, therefore the materials were considered to lose approximately half of their initial weight.

In order to evaluate how bio-stabilized materials contribute to the accumulation of heavy metals in soil, the initial concentration in the relevant soil horizon \( C_{\text{Bi,t}} \) was considered to be null. Results show an increasing trend of heavy metal concentration in soil, which is strongly influenced by the type of material considered. Metals with a similar concentration value show a similar trend, like Ni in all the three investigated samples. MBTW trends confirm that aerobic bio-stabilization of mechanically selected municipal waste produces a material with a higher metal content which may theoretically lead to exceed the threshold values for reuse in residential sites but only for very long application timeframes (i.e. 175 years for Pb). In 50 years, the total metal content would appear not to exceed the Italian soil contamination threshold values for residential use (Italian Decree N 152, 2006). Figure 2 shows how the initial concentration of a metal in the soil horizon can influence the results, with Cu as an example.
Taking into account in the mass balance of the initial metal content in the soil results in an increase of the metal concentration in the relevant soil horizon, but also in a slightly slower increase of metal accumulation over time. It is important to highlight that Equation 1 can be used to estimate the maximum value of concentration in the relevant soil horizon for \( t \to \infty \) (Equation 5).

\[
C_{B_{o,t}} \approx \frac{(C_{Samp} \times M \times 0.1 \times t)}{(M \times A_{long} \times 0.1 \times t)} = \frac{C_{Samp}}{A_{long}} \text{ for } t \to \infty \quad (5)
\]

The maximum value of concentration in soil depends only on \( A_{long} \); it means that concentrations approximately double for \( t \to \infty \).

\[
C_{B_{o,\infty}} \approx 1/0.519 C_{Samp} = 1.93 C_{Samp} \text{ for MBT W}
\]
\[
C_{B_{o,\infty}} \approx 1/0.445 C_{Samp} = 2.25 C_{Samp} \text{ for Compost A}
\]
\[
C_{B_{o,\infty}} \approx 1/0.514 C_{Samp} = 1.95 C_{Samp} \text{ for Compost B}
\]

Anyhow, it should be noted that metal accumulation calculated on the basis of Equation 1 should be considered as a first conservative estimate, since owing to rain water infiltration in the soil layer, metals, salts and other constituents are gradually leached from the biostabilised materials, which determines a decrease over time of their total content in the amended soil.

**Leaching behavior**

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**Table 1.** Results (mean ± standard deviation) of the samples characterization (Pantini et al., 2015, Lombardi et al., 2016, Di Lonardo et al., 2016)

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Solid content</th>
<th>Eluates from column test (L/S =10)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>MBTW</td>
<td>Compost A</td>
</tr>
<tr>
<td>Ash (%)</td>
<td>45.8 ± 1.6</td>
<td>32.7 ± 0.7</td>
</tr>
<tr>
<td>VS (%)</td>
<td>54.2 ± 1.6</td>
<td>67.3 ± 0.7</td>
</tr>
<tr>
<td>TOC (%)</td>
<td>27.0 ± 0.5</td>
<td>25.2 ± 0.8</td>
</tr>
<tr>
<td>Cu (mg/kgTS)</td>
<td>172 ± 110</td>
<td>57.2 ± 2.1</td>
</tr>
<tr>
<td>Ni (mg/kgTS)</td>
<td>15.7 ± 0.4</td>
<td>16.3 ± 2.0</td>
</tr>
<tr>
<td>Pb (mg/kgTS)</td>
<td>350 ± 120</td>
<td>25.9 ± 0.7</td>
</tr>
<tr>
<td>Zn (mg/kgTS)</td>
<td>370 ± 7</td>
<td>164 ± 3</td>
</tr>
</tbody>
</table>

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**Figure 2.** Metal accumulation in the soil over the long term, at different initial concentration values

\( (C_{B_{o,t}} = 50 \text{ mg/kgTS for Cu}) \)

**Figure 3.** Metal release in solution, resulting from percolation leaching tests

As can be noted, notwithstanding the different initial content of potential contaminants in the three types of biostabilised materials, their leaching trends as a function of the L/S ratio were quite similar (see e.g. the leaching curves resulting for Pb). However, also in this case the highest concentrations were generally retrieved in the leachate of the MBT waste, especially at low L/S ratios. Table 3 shows the time, calculated through Equation 4...
needed to reach the L/S of the percolation tests, assuming the application of 1 kg of material to 1 m² of soil. As can be noted, for the assumed conditions the resulting infiltration rate leads to achieve a L/S of 10 l/kg in just over a year.

Table 3. Time to reach the investigated L/S assuming to apply 1 kg of material to 1 m² of soil (Average annual rainfall \( P = 77.2 \text{ cm/year}; \) predominant soil type: Silt; horizon thickness \( h = 30 \text{ cm} \))

<table>
<thead>
<tr>
<th>Years</th>
<th>0.21</th>
<th>0.42</th>
<th>0.63</th>
<th>0.84</th>
<th>1.05</th>
</tr>
</thead>
<tbody>
<tr>
<td>L/S (l/kg)</td>
<td>2</td>
<td>4</td>
<td>6</td>
<td>8</td>
<td>10</td>
</tr>
</tbody>
</table>

Conclusions

The results of this preliminary study indicate that heavy metal concentrations may progressively increase in soils due to the application of biostabilised materials. The total metal content strongly influences pollutants' accumulation in soil, but it is only one of the factors among others influencing potential contamination. In fact, organic matter can modify the soil structure, especially considering the degradation that characterises this fraction during the long term. In addition, it should be considered that metals may be released over time due to leaching upon contact with rainwater or uptaken by vegetation. The mobility of potential contaminants is influenced by the nature of the bio-stabilized waste, but may also depend upon the characteristics of the soil to which they are added and from the intensity of the annual precipitation on the investigated area. Future studies will address the modification of the model employed in this work for the evaluation of metal accumulation in soils amended with biostabilised materials in order to possibly take into account of the above mentioned phenomena (leaching in particular) and assess also the potential impacts of the application of biostabilised materials to soil on groundwater quality.

References


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